



## Neutronic analysis of a fuel element with variations in fuel enrichment and burnable poison

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### ABSTRACT

In this work, the goal was to evaluate the neutronic behavior during the fuel burnup changing the amount of burnable poison and fuel enrichment. The analyses used a 17 x 17 PWR fuel element, simulated using the 238 groups library cross-section collapsed from ENDF/BVII.0 and TRITON module of SCALE 6.0 code system. The results confirmed the effective action of the burnable poison in the criticality control, especially at Beginning Of Cycle (BOC) and in the burnup kinetics, because at the end of the fuel cycle there was a minimal residual amount of neutron absorbers ( $^{155}\text{Gd}$  and  $^{157}\text{Gd}$ ), as expected, showing the burnup of the Gd in the simulation methodology adopted. Furthermore, the results show that increasing the Gd insertion percentage does not change its final residual amount. At the end of the cycle, the fuel element was still critical for all the simulated situations, which indicates the possibility of extending the fuel burnup.

*Keywords:* neutronic analysis, fuel element, burnable poison.

## 1. INTRODUCTION

The burnable poison (or simply poison) is a substance, which has a high neutron absorption cross-section, which reduces the reactivity of a reactor core [1]. These neutron absorbers are chosen because they transmute by neutron capture into isotopes with low capture cross sections, somewhat faster than fuel burnup, thus leaving a residual minimum amount of burnable poison at the end of the fuel cycle [2]. Such characteristics of burnable poison improve fuel utilization, contributing to a more homogeneous power distribution into the reactor core and are able to control nuclear reactivity.

Burnable poisons are rare on earth and they are particularly useful for the control of nuclear reactivity, among which are the elements Samarium (Sm), Europium (Eu), Dysprosium (Dy), Erbium (Er) and Gadolinium (Gd).

The presence of burnable poison in adequate amounts reduces the use of control rods [3]. This practice reduces the amount of actinides and fission products, and does not change the thermal conductivity [4]. The burnable poisons remove neutrons by absorption and thus effectively reduce the excess of reactivity in the nuclear core. This effect is generally desirable at BOC, due to the excess of reactivity at load the core with fresh fuel, being necessary a high concentration of burnable poisons. The best way to improve the fuel utilization is based on the burnup extension and poison kinetics at BOC, since the lowest remaining residual concentration of the burnable poison is expected at the end of the cycle in order to stop neutrons absorption and to reduce any core excess reactivity.

Cochran and Tsoufanidis (1999) [5] reported that gadolinium (Gd) seems to be more attractive because it can be mixed directly with  $\text{UO}_2$ . It has several isotopes and the natural abundance of  $^{155}\text{Gd}$  and  $^{157}\text{Gd}$  are 14.7% and 15.7%, respectively. Their absorption cross sections for thermal neutrons are  $5.8 \times 10^4$  and  $2.4 \times 10^5$  barns, respectively.

A relevant way to improve nuclear fuel efficiency is using Gd by enriching the percentage of natural isotopes  $^{155}\text{Gd}$  and  $^{157}\text{Gd}$  [6]. This enrichment can eliminate the presence of parasite absorber at EOC [7]. Although Schlick (2001) [8] reported that the contribution of  $\text{Gd}_2\text{O}_3$  in values close to 2% does not affect the thermal conductivity of the fuel, it is known that the amount used in PWR is generally higher than these values.

The aim of this work was to evaluate the neutronic behavior during burnup changing the amount of burnable poison and fuel enrichment. Neutronic parameters such as infinite multiplication factor and composition of burnable poison have been analyzed during burnup and at EOC. The gadolinium pins were simulated in a homogeneous mixture with uranium oxide ( $\text{UO}_2$ ) containing 0.2% of  $^{235}\text{U}$  and with different proportions of gadolinium in the mixture of  $\text{UO}_2 + \text{Gd}_2\text{O}_3$ , 4, 6 and 8%. Two enrichment, one of 3.25% and other of 4% of  $^{235}\text{U}$ .

## 2. METHODOLOGY

### 2.1. Description of the modeled system

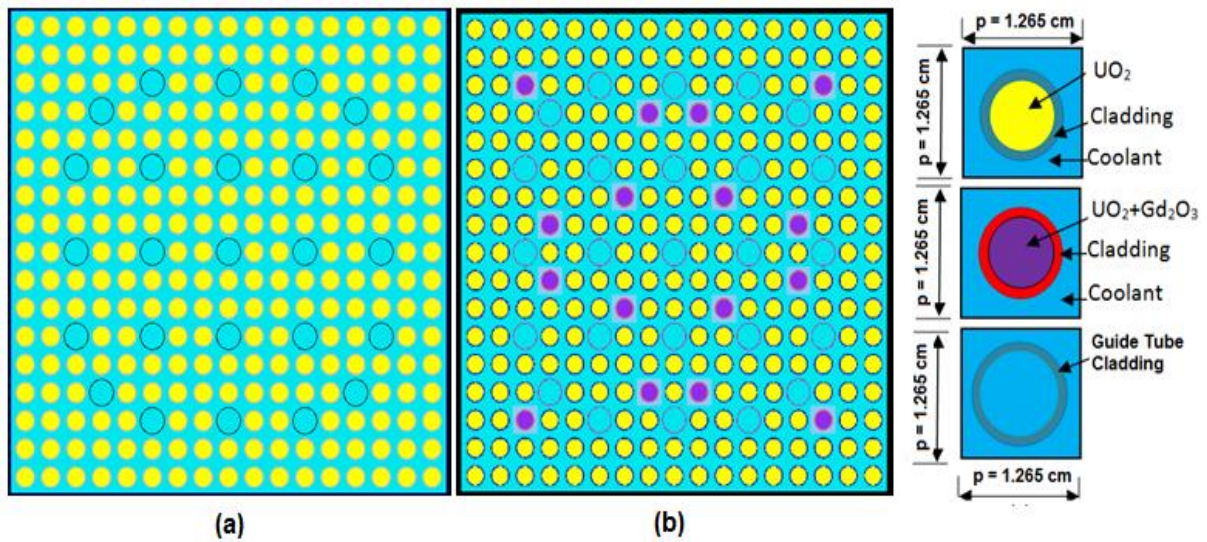
The simulations were carried out considering a Pressurized Water Reactor (PWR) fuel element arranged on an assembly of 17 x 17, with a central guide tube, totalizing 24 guides tubes [9], without boron dilution. This fuel assembly was simulated for two different cases: one without Burnable Poison Rods (BPR) and the other with 16 BPR. The rods of  $\text{UO}_2$  have different enrichments as described in Table 1, according to the literature [9 and 10]. For the benchmark fuel element analysis was used the nuclear code SCALE 6.0 [11], although 238 groups collapsed from ENDF/BVII.0 library of cross section [12].

**Table 1:** Fuel rods and 16 Burnable Poison Rods

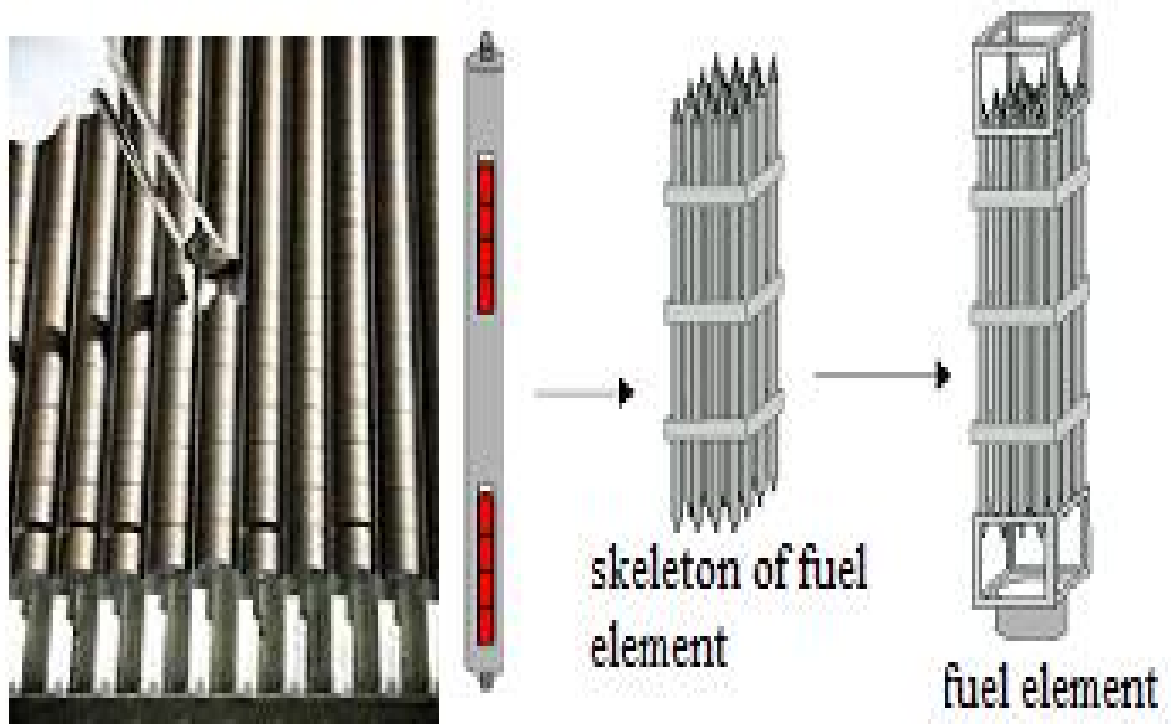
$\text{UO}_2$ with enrichment ( $^{235}\text{U}$ )	$\text{UO}_2$ (0.2% $^{235}\text{U}$ ) + $\text{Gd}_2\text{O}_3$
3.25%	2.00%
	4.00%
	6.00%
	8.00%
4.00%	2.00%
	4.00%
	6.00%
	8.00%

Figure 1 shows fuel rod assembly with guide tubes, with 16 BPR, and without BPR, and was generated using the SCALE 6.0 code. To calculate the infinite multiplication factor ( $k_{\text{inf}}$ ), the geometry of the bundle model was reflected from all sides. In this way, neutrons are not allowed to escape from the system. Figure 2 shows pellets fuel, fuel rod, and fuel element.

**Figure 1:** (a) Fuel rod assembly geometry with the guide tube and without BPR. (b) Fuel rod assembly geometry with the guide tube and 16 BPR.



**Figure 2:** Pellets fuel and rod with stacked pellets.



[13]: [http://www.inb.gov.br/ptbr/WebForms/Interna2.aspx?secao\\_id=58](http://www.inb.gov.br/ptbr/WebForms/Interna2.aspx?secao_id=58) access (2013).

Table 2 presents other parameters used in modeling of the fuel element according to the literature [9], considering the number of BPR inserted.

**Table 2:** Fuel element parameters

DESCRIPTION	VALUE
Active length fuel Rod	365.7 cm
Active length guide tube	365.7 cm
Fuel radius	0.412660 cm
Radius cladding fuel (Zircaloy)	0.474364 cm
Radius coolant inside guide tube	0.572940 cm
Radius guide tube	0.613010 cm
Pitch (p) rods	1.265 cm
Pitch fuel elemento	21.505 cm
Fuel temperature (Zircaloy)	873 K
Burnable Poison Rods	WBPR and 16*
Cladding temperature (Zircaloy)	673 K
Coolant temperature	573 K
Power concentration	38 W/gU

\*changes made relative to reference [9]

Using the same methodology and maintaining the same geometry, 16 rods of UO<sub>2</sub> were replaced by burnable poison. The first case studied the arrangement without BPR and the second one with 16 BRP, with different gadolinium percentages 2.00%, 4.00%, 6.00% and 8.00%, as mentioned in Table 1.

## 2.1. Simulations: fuel depletion with SCALE 6.0

The SCALE code estimates the infinite multiplication factor ( $k_{inf}$ ) with the respective standard deviation of the model ( $\sigma_{ST}$ ). This works aimed to evaluate: (a) the criticality of the system with different enrichments and different percentages of burnable poison during fuel depletion and (b) the impacts of burnable poison in the  $k_{inf}$ .

For fuel depletion calculation, TRITON module [14] was used through T6-depl command with 10000 particles and 2200 generations. The library ENDF/BVII.0 was used with 238 collapsed groups (V7-238), because it presents less deviation from the average, besides being able to be used in the calculations during fuel evolution [15]. The specific power density was 38 W/gU during 789.48 days, producing an overall burnup of 30 GWd/tHM [9]. To analyze the burnup and the impact of burnable poison in the reactivity, the time was divided into small intervals, including periods of decay, as shown in Table 3.

**Table 3:** Division of the period of burnup and decay of fuel

Period	Cycles (days)	Decay (days)	Burnup GWd/MTU
1	50	30	5.7
	50		
	50		
2	100	66	11.4
	100		
	113.16		
3	113.16	299	12.9
	113.16		
Total	789.48	395	30.0

Equation 1 was used to calculate the absolute difference (Abs.diff.) of infinite multiplication factor values of simulated fuel element without insertion of burnable poison ( $k_{infWBP}$ ) and with the insertion of burnable poison ( $k_{infBP}$ ):

$$Abs. \text{ diff. (pcm)} = (k_{infWBP} - k_{infBP}) \times 10^5 \quad \text{equation (1)}$$

During fuel evolution, infinite multiplication factor ( $k_{inf}$ ) was compared as a function of gadolinium, especially  $^{155}\text{Gd}$  and  $^{157}\text{Gd}$ , as isotopes with the greatest abundance, 14.7% and 15.7% and the

highest absorption cross section for thermal neutrons equal to  $5.8 \cdot 10^4$  and  $2.4 \cdot 10^5$  barns, respectively [5].

### 3. RESULTS AND DISCUSSION

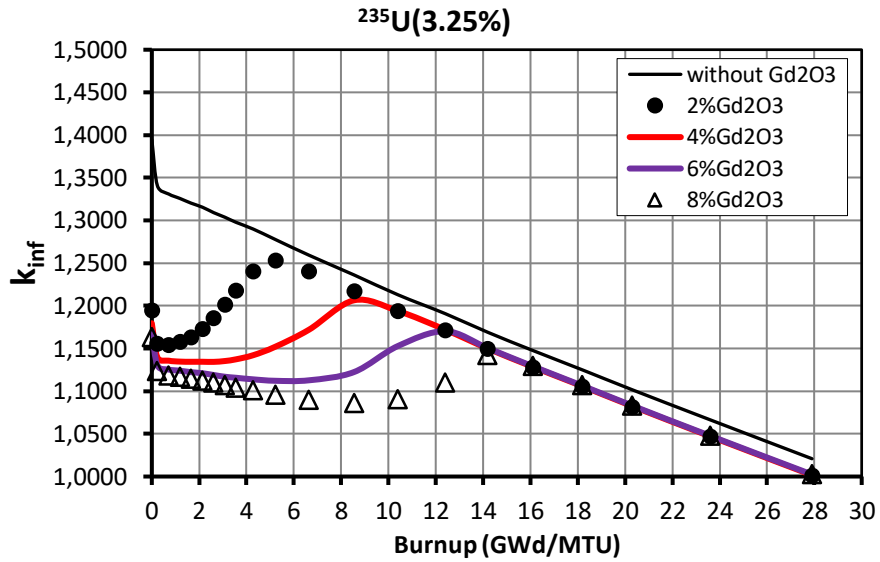
Figures 3 and 4 show the variations of  $k_{inf}$  values changing fuel enrichment and proportion burnable poison. The standard deviation estimated by the used code has a magnitude of  $10^{-4}$ . All cases, the main difference between graphics is predominant at the Beginning Of Cycle (BOC), period of effective action of the burnable poison.

It is important to emphasize that the value of  $k_{inf}$  is always lower in all simulations, during the period when there is a higher concentration of burnable poison, as shown in Figures 3 and 4. This allows the reduction of control rods at the Beginning Of Cycle (BOC).

Figures 3 and 4 show another relevant fact, the evolution of  $k_{inf}$  values began to have the same profile of the fuel element Without Burnable Poison (WBP) from 14.0 GWd /MTU, suggesting the possibility of fuel burnup extension, since the fuel element is still critical.

Figures 3 and 4 also show a sharp decrease in  $k_{inf}$  value and some peaks at different burnup points, which can be justified by the analysis of the gadolinium isotopes  $^{155}\text{Gd}$  and  $^{157}\text{Gd}$  evolution during burnup, as shown in Figures 5 and 6. The  $k_{inf}$  curve variations move from 2.0 GWd/MTU to 14.0 GWd/MTU for the fuel with uranium enrichment at 3.25%, and from 2.0 GWd/MTU to 16.0 GWd/MTU for the fuel with uranium enrichment at 4%. where all simulated cases with  $\text{Gd}_2\text{O}_3$  insertion have the same linear profile and parallel to the simulated cases without insertion of burnable poison. This behavior shows that increasing the Gd insertion percentage, there is a displacement of the return point to the behavior of the curve without gadolinium, showing the effectiveness of the burnable poison until approximately by half of the burnup. Nevertheless, the increase of Gd insertion percentage does not change its final residual amount.

**Figure 3:** Comparison of infinite multiplication factor with 3.25% enrichment of  $^{235}\text{U}$ .



**Figure 4:** Comparison of infinite multiplication factor with 4.00% enrichment of  $^{235}\text{U}$ .

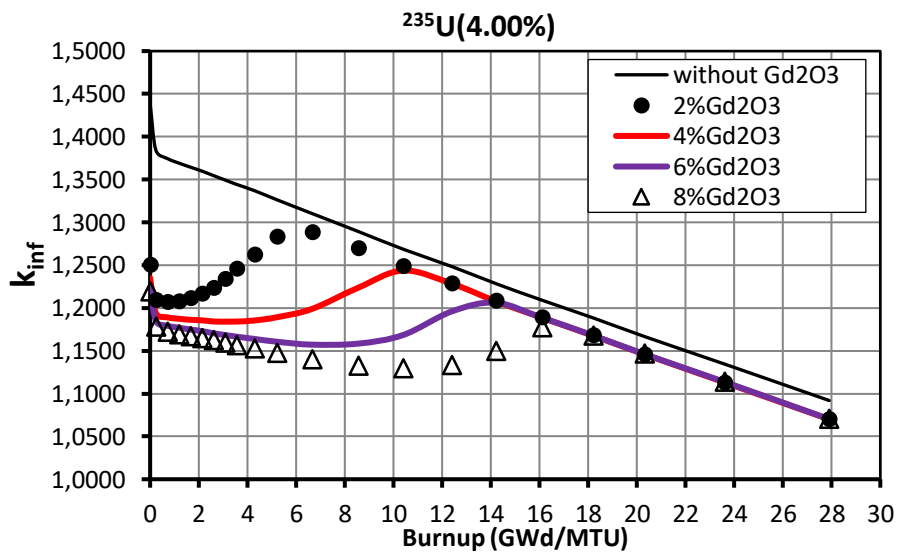


Table 4 shows the initial and final composition of  $^{155}\text{Gd}$  and  $^{157}\text{Gd}$ , during fuel burnup. As observed the final amount is small compared to one at BOC.

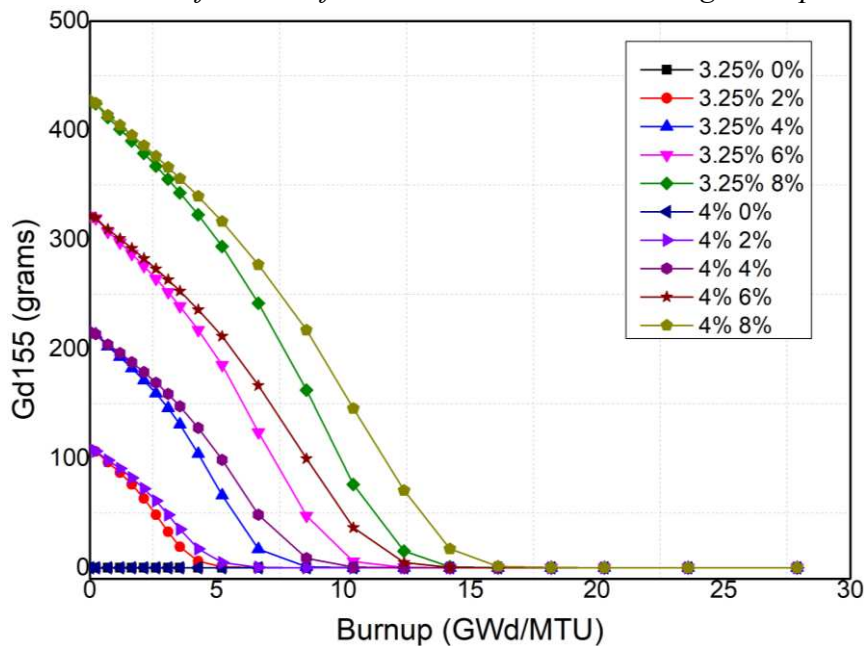
**Table 4:** Compositions in grams of  $^{155}\text{Gd}$  and  $^{157}\text{Gd}$  in BOC and EOC



UO <sub>2</sub> with enrichment ( <sup>235</sup> U)	UO <sub>2</sub> (0.2% <sup>235</sup> U)+Gd <sub>2</sub> O <sub>3</sub>	Compositions (g) <sup>155</sup> Gd		Compositions (g) <sup>157</sup> Gd	
		BOC	EOC	BOC	EOC
		3.25%	2.00%	230.8	0.3885
4.00%	459.8		0.4861	486.2	0.2042
6.00%	687.2		0.5847	726.6	0.2517
8.00%	912.8		0.6840	965.2	0.2941
4.00%	2.00%	237.9	0.3748	251.5	0.1522
	4.00%	474.0	0.4830	501.2	0.2150
	6.00%	704.8	0.5908	749.1	0.2677
	8.00%	941.1	0.7002	995.1	0.3154

Figure 5 and Fig. 6 show the behavior of <sup>155</sup>Gd and <sup>157</sup>Gd during burnup and can be related to the intervals of  $k_{inf}$  values. As expected, the gadolinium amount decreased. <sup>155</sup>Gd and <sup>157</sup>Gd after the total burnup are still present, but in much smaller quantities than those present at BOC. The <sup>155</sup>Gd level reached a stable amount near of burnup of 15.0 GWd/MTU, while regarding to <sup>157</sup>Gd, this occurred near to burnup 10.0 GWd/MTU.

**Figure 5:** Behavior of <sup>155</sup>Gd with <sup>235</sup>U enriched to 3.25% and 4.0%, without Gd<sub>2</sub>O<sub>3</sub> and with variations of Gd<sub>2</sub>O<sub>3</sub> of 2%, 4%, 6%, and 8%, during burnup.



**Figure 6:** Behavior of  $^{157}\text{Gd}$  with  $^{235}\text{U}$  enriched to 3.25% and 4.0%, without  $\text{Gd}_2\text{O}_3$  and with variations of  $\text{Gd}_2\text{O}_3$  of 2%, 4%, 6% and 8%, during burnup.

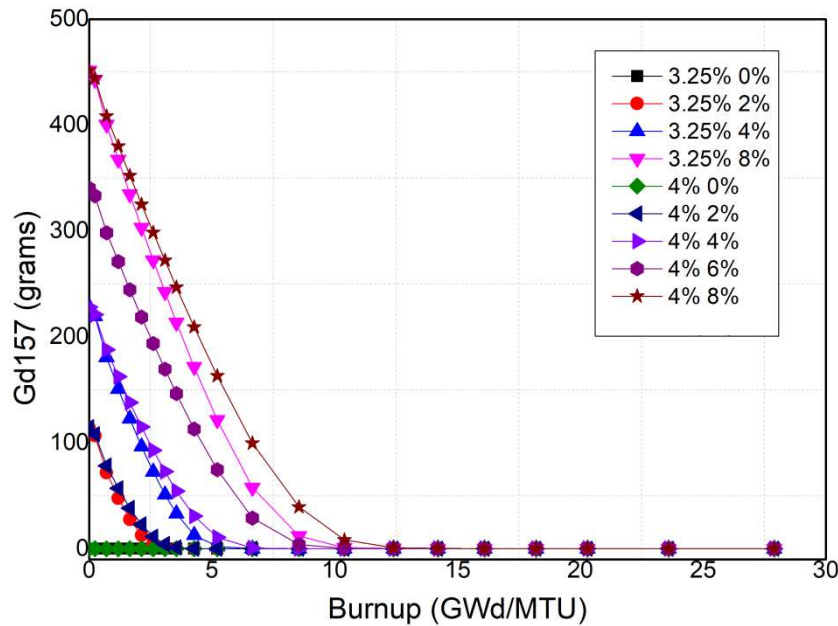
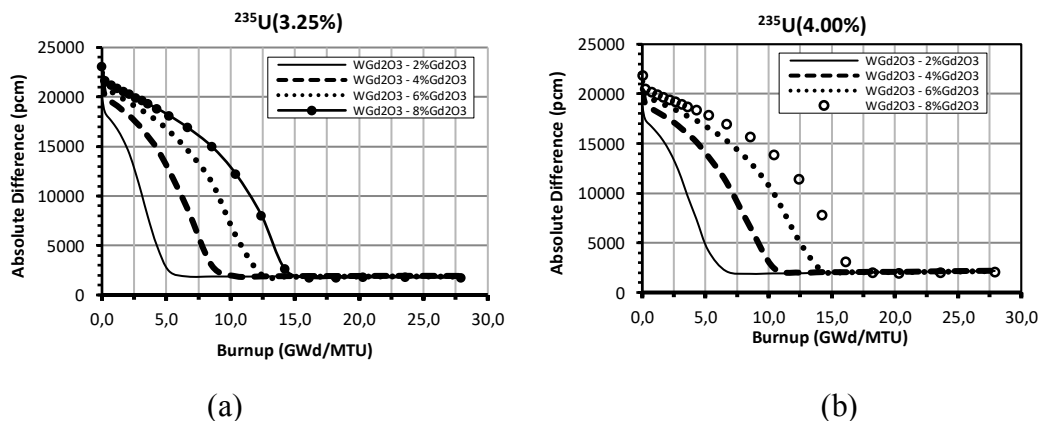


Fig. 7 shows the absolute difference between the  $k_{inf}$  values with the enriched fuel for 3.25%, 4.00%, and  $\text{Gd}_2\text{O}_3$  variations. The biggest absolute difference throughout burnup occurs in the range of 0.0 to 15.0 GWd/MTU, where it has a higher amount of burnable poison acting. From this interval the behavior is stable and it is no longer possible to identify any difference. Thus indicating, that there is only a residual quantity of burnable poison in comparison with the amount inserted at the beginning of the cycle.

**Figure 7:** (a) Absolute difference between  $k_{inf}$  values with fuel enriched to 3.25% and with variations of  $\text{Gd}_2\text{O}_3$  and (b) absolute difference between  $k_{inf}$  values with fuel enriched to 4.00% and with variations of  $\text{Gd}_2\text{O}_3$



#### 4. CONCLUSION

This neutronic study confirmed the importance of burnable poison in the control of reactivity without the use of control rods, especially at the beginning of the cycle, when there is the greatest excess of reactivity during all the burnup.

This study showed that the consumption of burnable poison does not occur homogeneously, because, at the end of the cycle, there is a larger amount of  $^{155}\text{Gd}$ , not maintaining the observed proportion at the beginning of the cycle.

This neutronic analysis confirmed that there was good synchrony in the burnup kinetics of the burnable poison, even with the different percentages used, as it presented at the end of the cycle a residual amount comparable to the simulations without the insertion of burnable poison. Nevertheless, the increase of Gd insertion percentage does not change its final residual amount.

The next study is to make comparisons of results with other nuclear codes, such as MCNP-X and Monteburns, to increase fuel enrichment, make burns higher than that of this study, vary the amount of burnable poison rods, simulate the fuel element with the use of burnable poison enriched, in order to verify its efficiency.

The goal will be:

- to compare the values of  $k_{\text{inf}}$  and actinides generated when the control rods are moved, with the values using the different percentages and amounts of burnable poison rods;
- to establish the best combination of the use of control rods, the percentage, and quantity of burnable poison rods and actinide generation;
- to simulate the core of a PWR reactor with the best combinations of use of control rods and burnable poison.

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## REFERENCES

1. CNEN-NE-1.27, INSTALAÇÕES NUCLEARES, “Garantia de Qualidade na aquisição, projetos e fabricação de elementos combustíveis”, Rio de Janeiro, Resolução 02/95, Publicação D.O.U. 01/09/95, Resolução 15/95, Publicação D.O.U. 21/09/99.
2. DUDERSTADT, JAMES J.; HAMILTON, LOUIS J., **Nuclear Reactor Analysis**, JohnWiley & Sons, Inc., New York, 1976.
3. WAGNER, J. C.; PARKS, C.V., “Parametric Study of the Effect of Burnable Poison Rods for PWR Burn up Credit”, NUREG/CR-6761, ORNL/TM-2000/373, Oak Ridge National Laboratory, (2002).
4. IWASAKI, KOUTA.; MATSUI.; YANAI, KOICHI.; YUDA, RYOUICHI.; ARITA, YUJI.; NAGASAKI, TAKANORI.; YOKOYAMA, NOBORU.; TOKURA, ICHIRO.; UNE, KATSUME.; HARADA, KENICHI, “Effect of Gd<sub>2</sub>O<sub>3</sub> Dispersion on the Thermal Conductivity of UO<sub>2</sub>”, **Journal of Nuclear Science and Technology**, Vol. 46, number 7, pag. 673-676 (2009).
5. COCHRAN, ROBERT.; TSOUFANIDIS, NICHOLAS., **The nuclear fuel cycle: analysis and management**. 2<sup>nd</sup> ed., American Nuclear Society, 1999, La Grange Park, Illinois, USA.
6. YILMAZ, SERKAN.; IVANOV, KOSTADIN.; LEVINE, SAMUEL.; MAHGEREFTEH, MOUSSA., “Development of enriched Gd-155 and Gd-157 burnable poison designs for a PWR core”, **Annals of Nuclear Energy** 33 439-445 (2006).
7. BEJMER, KLAES-HÅKAN.; SEVEBORN, OLA, “Enriched Gadolinium as Burnable Absorber for PWR”, La Grange Park : American Nuclear Society, Lagrange Park, IL, 25-29 de April de 2004, **PHYSOR 2004 – The Physics of Fuel Cycles and Advanced Nuclear Systems: Global Developments** Chicago, Illinois.
8. SCHLIECK, M.; BORGER, H. –D.; NEUFERT, A., “Optimized gadolinia concepts for advanced in core fuel management in PWRs”. **Nuclear Engineering Designs** 205, 191-198, (2001).
9. OECD, Organisation for Economic Co-Operation and Development. “Burn-up Credit Criticality Benchmark - Phase II-D - PWR-UO<sub>2</sub> Assembly Study of Control Rod Effects on Spent Fuel Composition”, NEA N° 6227, ISBN: 92-64-02316-X, France, (2006).
10. DAVID BERNARD and ALAIN SANTAMARINA, “Qualification of gadolinium burnable poison: Interpretation of MELUSINE/GEDEON-II spent fuel analysis”, **Annals of Nuclear Energy** 87 (2016) 21-33.

11. S. M. Bowman, KENO-VI Primer: “A Primer for Criticality Calculations with SCALE/KENO-VI Using GeeWiz”. Oak Ridge, Tennessee, USA: ORNL/TM-2008/069 (2008).
12. BOWMAN, S. M. e DUNN, M. E. SCALE Cross-section Libraries, Oak Ridge, Tennessee, USA: ORNL/TM-2005/39, Version 6, Vol. III, Sect. M4 (2009).
13. [http://www.inb.gov.br/ptbr/WebForms/Interna2.aspx?secao\\_id=58](http://www.inb.gov.br/ptbr/WebForms/Interna2.aspx?secao_id=58). Last access (2013).
14. M. D. DEHART. TRITON: “A Two-dimensional Transport and Depletion Module for Characterization of Spent Nuclear Fuel”. Oak Ridge, Tennessee, USA : ORNL/TM-2005/39, Version 6, **Vol. I**, Sect. T1 (2009).
15. FARIA, ROCHKHUDSON BATISTA DE. Carbetto de silício reforçado com fibras de Hi-Nicalon tipo S como revestimento de reatores PWR – avaliação neutrônica/Rochkhudson Batista de Faria – 2017. Tese (doutorado) Universidade Federal de Minas Gerais, Escola de Engenharia.